**Wet-high intensity magnetic separation of magnesite ore waste**

Ahmet ATASOY

Faculty of Technology, Department of Metallurgy and Materials Engineering, University of Applied Sciences of Sakarya, 54187 Sakarya - Turkey

E-mail: aatasoy@sakarya.edu.tr

**Abstract**

In this paper, investigation was carried out on a wet high intensity magnetic separation of the waste of magnesite ore where is stocked in open pit magnesite mine. The as received sample was subjected to physical, chemical, thermal and phase characterizations. The waste of magnesite ore sample containing 77.69 % MgCO3 and considerable amount of 3.14 % Fe2O3. The unwanted silica iron impurities were removed and the high grade magnesite was obtained trough experiments. The results showed that the high grade of magnesite was obtained at 1.8 T after the twice passing of the non magnetic portion of the processed sample. It is possible to upgrade magnesite to 91.03 % and reduce iron content to 0.32 % after the magnetic separation. After the calcination process at 1000 ˚C, the sample showed 52 % of loss of ignition and yielded 85.39 % MgO with a 0.32 % Fe2O3. The final product can be used in chemical and metallurgical applications where high magnesia content requires. The experiment results provide useful information on the wet magnetic separation of magnesite waste.

**Key words:** Magnesite waste, beneficiation, magnetic separation, calcination, magnesia,

**1. Introduction**

Magnesite is the major mineral of magnesium, the other minerals are talc, brucite and dolomite [1].Other impurity minerals in magnesite ore are quartz, apatite and small amount of iron. It is formed through the carbonation of magnesian serpentine in the presence of water and carbon dioxide under moderate temperature and pressure. Chemical composition of magnesite ore is complex and varies country to country. Depending on magnesite ore, it contains MgO (42-47 %), CaO (1.0-2.0 %), SiO2 (1 %), Al2O3 (1 %), Fe2O3 (1 %) and 50 % ignition loose. According to magnesia content of magnesite ore can be classified into three groups are high (MgO > 46 %), middle and low (MgO < 43 %) grades [2].

Due to physicochemical properties, magnesite is used in wide range of industrial applications including ceramic, metallurgy, cement, fertilizer, animal feed or refractory. More than 90% is used for sinter and caustic magnesia production as a fire resistance and slag materials in metallurgical application of steels,chemical, glass industries [3].

Magnesite ore occurs from ultrabasic and ultramafic peridoties in cryptocrystalline type ore.Turkey is one of the largest magnesite ore producer and refractory exporter country in the world (7 % of the total refractory production). The country has large magnesite ore deposits (approximately 2 % of the world total) and are number of operators and exporter of magnesite ore. Approximately, 2 million tons of magnesite ore is mined in the country using for magnesia compounds such as dead burned, fused or chemical applications. Mining of magnesite ore in the country is carried out by open mining method in which the ore was beneficiated by hand/optical sorting, crushing screening, scrubbing and magnetic separation are used upgrading [4]. High calcium and silica content is restricted purification of magnesite. Therefore, it is very important to reduce unwanted oxides in it. After beneficiation processes, magnesite is subjected to calcination operation. According to calcination temperature, magnesia is named such as reactive magnesia (700-1000 ˚C), dead/hard burned magnesia (1000-2200 ˚C) and fused magnesia (above 2750 ˚C).

Magnetic separation is based on a direct physical separation method of minerals in magnetic field. Magnetic properties of minerals can be divided into three basic groups, ferromagnetic, para magnetic and diamagnetic. Magnetic susceptibility differences in particles sizes is accomplished wet or dry, at various intensities and in different basic machine configurations. Modern industrial application can be found different types. Choosing of magnetic separation method depends on many processing parameters including ore or mineral type and compositions and grades, particle size as well as their magnetic susceptibility. Addition of these, production and marketing factors are considered.

Magnetic separation has been used to upgrade and beneficiate variety of industrial minerals. First application on industrial minerals of magnetic separation process is to remove of iron oxide content such as hematite-limonite [5], taconite [6], pyrite (FeS2), pyrohiotite (Fe7S8) [7]. It is dominant separation process in iron containing ores. There were well explained the principle of magnetic properties of materials [8, 9] and applications in the literature [10]. Today, it is used from metallurgical, steels, scrap, food, medical, drug delivery or bio applications [11].



**Figure 1** Flowsheet for magnesia processing.

A flowsheet for the processing of magnesite ore is given in Figure 1 that is generally accomplished by crushing/screening, hand sorting and dry magnetic separation. In addition those methods, froth flotation, leaching, agglomeration, coagulation or fluctuation methods can be used. Selection of beneficiation methods depends upon the mineralogical composition and the texture of the ore. To upgrade wanted content or to recovery of it, number of physical separation methods are applied such as froth flotation [12, 13], electrostatic [14], gravity [15, 16], or magnetic [17]. Each methods has advantages and disadvantages on applications, for example, flotation process treats very fine particles but needs some chemical agents and water which used media may creates environmental pollution and problems. Electrostatic route is environmentally friendly than flotation method from this point of view.

Extraction of magnesite from ore generates huge amount of soil waste. Due to availability of huge amount of magnesite ore tailing waste, it is important to utilize these waste as new magnesite potential source. Therefore the main objective of the present study is the characterization and the beneficiation of magnesite waste. High intensity wet magnetic separation was applied for the separation of magnetic and non magnetic fractions of the sample.

The present paper describes the characterization of magnesite tailing from Kütahya Magnesite Cooperation (KUMAS) Company and the application of the high intensity wet magnetic separation method was used to recovery of magnesite below -3.00 +0.100 mm size fraction. Characterizationwas performed with thermal analysis, X-ray diffraction, scanning electron microscope, elemental analysis and infrared spectroscopy.

**2. Experimental**

**2.1. Materials**

The magnesite tailing was provided by the KUMAŞ Magnesite Inc. that wasprivatized in 2012, dominates in the magnesite mining industry [18]. ROM magnesite ore is beneficiated by hand sorting and dry magnetic separation at the mine sites for pre-concentration. Then it subjected to final beneficiation by high intensity dry magnetic separation. Depending on the impurity content of magnesite ore, the company has seven magnesite products, such as supper (Fe2O3 0.00 - 0.24 %), extra (Fe2O3 0.25 - 0.29 %), special (Fe2O3 0.30 - 0.33 %), quality 1-4(Fe2O3 0.34 - 0.72 %). It produces 35 thousand tons of fused magnesite (FM), 275 thousand tons of dead burned magnesite (DBM) and 55 thousand tons of caustic calcinated magnesia (CCM). Magnesite tailing from the plant contains significant amount of magnesite as a low grade where is deposited in the plant to utilize the tailing in order to recovery of valuable oxide, to reduce storage and environmental problems. At the same time, tons of magnesite ore waste material has been stocked every year that damages the environment. A flowsheet was presented in Figure 2 for the experimental works.



**Figure 2** The flowsheet used for the characterization and the high intensity wet magnetic separation of the magnesite waste sample.

**2.2. High intensity wet magnetic separator**

When compare dry and wet magnetic separation techniques, conventionally, wet magnetic separation is used at finer size fractions, which is decreased impurity, high purity and better quality of products.

A high gradient electro magnet was used for the beneficiation of fine size -3.00 +0.10 mm magnesite tailing. The magnetic separation experiments were carried out at the research laboratory of AKSA Magnet at Sakarya in Turkey. The separator (HIWMS) consists of a separation canister packed with a strong ferromagnetic iron ball matrix. A magnetic field is trapped on the ball matrix which collect the magnetic particle and the non-magnetic portion is collected downstream. The intensity of the magnetic field developed between the coils was measured by means of Tesla.

Approximately, 50kg sample was made into slurry of desired initial pulp density with water (1:1 ratio). The slurry was stirred and passage through magnetic separator, the nonmagnetic slurry portion was collected downstream. The trapped magnetic portion was recovered from the ball matrix, after shutting down of the high intensity wet magnetic separator (HIWMS).

**2.3. Analysis and characterizations**

The particle size range of the magnesite tailing received was -3.00 +0.10 mm. The sample sieving was carried out on six different size fractions between -3.00 to + 0.10 mm, using a laboratory sieve vibrated for 5 min. and then the amount of material retained on each sieve was weighed.

For the determination of mineral phases in the received samples and the products, X-ray diffraction method (D/max Rigaku, Japan) was used at the condition of Cu Kα radiation (λ=0.15418 nm) with a step size of 0.02˚ (2θ) and a scanning rate of 2˚ min-1. Energy dispersive analytical X-ray (EDAX) was also used for basic chemical analysis.

Thermal analysis of the mixture was performed on a simultaneous thermal analyzer (Netzsch STA 400, Germany). TG/DTA was performed in an alumina crucible, under nitrogen atmosphere in the temperature range of 20-1450 ˚C and heating rate of 10 ˚C/min.

**2.4. Calcination and calcination behavior**

Calcination is pyrometallurgical process which depends on temperature, time, pressure and particle size and heating rate. It is heating process of carbonates, hydroxides, sulfate, nitrate,, acetate are converted into their oxide forms in a furnace at high temperatures in air. Thermal treatment of magnesite is important process in preparation of pure magnesia that is used for any metallurgical or chemical applications. Magnesite decomposition drives off CO2 and produces magnesia. According to the thermal treatment temperature can be classified into three products of magnesia are calcinated, dead burned and fused magnesia. Conventionally calcination of process for magnesite is carried out at temperature up to 1000 ˚C. The main objective of behind thermal treatment of magnesite sample are removing of volatile content of water, organic content and dissociation of carbonate forms of the defined sample that goes to calcination.

**3. Results and Discussions**

**3.1. Characterization of the magnesite waste**

Magnesium carbonate (MgCO3) occurs naturally as the mineral magnesite in two physical forms, macro crystalline (spathic) and cryptocrystalline (amorphous, compact) [4]. It was reported that, Turkey mostly has cryptocrystalline magnesite reserves. Cryptocrystalline magnesite is generally of higher purity than macro crystalline magnesite and generally contains less iron oxide [3, 4, 7, 18 ]. The magnesite deposit of the country are widely distributed and can be divided into two parts. The first part of the deposit is located from Kütahya to Eskişehir region and the second part is located in the east providence of Erzincan [7]. The ore deposits often occur as an alteration product in ultrabasic rocks, typically serpentine (magnesium silicate).

X-ray diffraction pattern of the received magnesite tailing sample was given in Figure 3. Magnesite exists in the shape of granularity and crystals in the ore. The main impurity minerals are dolomite, calcite, diabase, quartz and different forms of lizardite such as 1M (Mg3(Si2O5)(OH)4), 1T ( trigonal pyramids, Mg2.82Fe0.07Al0.09)(Si1.94Al0.06)O5(OH)4), and 2H (hexagonal plates, Mg2.83Fe0.05Al0.10)(Si1.93 Al0.07 )O5(OH)4). As expected, magnesite and lizardite were the second major phases in it. These impurities are important on successful mineral separation of any sample.



**Figure 3** XRD pattern of the as received magnesite waste sample.

It is known that, in magnesite refractories, magnesia and periclase are major phases. The composition of magnesite raw materials for producing of magnesia play critical effect on quality of magnesite refractories. Higher magnesia and higher calcia to silica ratio display the higher refractoriness, on the other side, the impurities such as iron and aluminium minerals have negative effect on magnesia refractories, since they lead formation of metallic iron which melts and creates holes that affect the refractoriness, sintering, mechanical and thermal stability of magnesite refractories.

The relative proportions of the particle size was determined by sieve analysis test. The collected data was presented in Table 1. The particle size rage of the sample was between -3.00 to 0.1 mm. As seen from it, the dominant particle size range was -2.00 +1.00 mm that corresponds to 40.21 % of the total retained quantity. The particle size of the second large portion corresponds to -1.00 +0.5 mm that equals to approximately ¼ of the retained quantity of the total.

**Table 1** Sieve analysis of the magnesite tailing sample.

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
| Sieve size (mm) | -3.00 +2.00 | -2.00 +1.00 | -1.00 +0.500 | -1.00 +0.250 | -0.5 +0.100 | -0.100 |
| Weight % | 12.21 | 40.21 | 26.73 | 13.82 | 4.95 | 2.08 |

In order to evaluate magnesia content of the tailing relating to the chemical analysis of the processed samples data collected from the X-ray fluoresce (XRF) method. Each data was in good agreement with others that were a linear relationships between them. The chemical composition of the magnesite tailing (T) sample was given in Table 2 at the first line. The main oxide was MgO in the form of magnesite with a percentage of 77.69 %, and the second oxide is silica with 12.10 % in the various minerals in form of serpentine, lizardite and quarts. The iron content of the received sample was 3.14 %. There were a numbers of trace impurities such as Al, Mn, K, Zn, Ni and Cr oxides less than 0.5 % in total.

**Table 2** XRF analysis (wt. %) of the received and the processed samples.

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| Samples | Mg\* | SiO2 | Ca\* | Fe2O3 | Al2O3 | NiO | Cr2O3 | MnO | K2O | ZnO | Mst. | Loi. |
| T | 77.69 | 12.10 | 6.68 | 3.14 | 0.19 | 0.10 | 0.10 | 0.06 | 0.01 | 0.003 | 4.67 | 37.01 |
| W | 62.46 | 26.02 | 3.52 | 6.96 | 0.49 | 0.20 | 0.19 | 0.11 | 0.08 | 0.005 | 5.05 | 17.02 |
| P | 91.03 | 3.92 | 4.58 | 0.32 | 0.05 | n. a. | 0.07 | 0.01 | n. a. | 0.002 | 3.31 | 48.00 |
| T : Magnesite tailing as received, W: Magnetic portion, P: Magnesite portion, Mst: Moisture content,Loi: Lost of ignition, \*forms in CO3 structure |

**3.2. High intensity wet magnetic separation**

Magnetic separation finds its application in the mineral industry, is commonly used method for removing of iron bearing minerals in ores. Today, high intensity wet magnetic separation method (HIWMS) offers potential for higher product purity and reduced operating and maintenance costs relative to alternative hand sorting, dry, physical, or gravity separation processes. The introduction of magnetic separators to the magnesite industry, to remove paramagnetic contaminants dramatically improved quality and doubled useful reserves worldwide. The process enables extraction from a solid/water suspension of superfine (even colloidal) particles that are only weakly magnetic.

Physical processing of Turkish magnesite from Kumaş by the high intensity wet magnetic separation is based on the removing of iron bearing minerals. As seen from the sieve analysis of the received magnesite ore tailing, the size range was -3.00 +0.1 mm. The sample was mixed with water in 1:1 ratio, a slurry obtained and then subjected to magnetic separation process at 1 T (Tesla) and 1.8 T (Tesla). After the process, the two samples, P was the non-magnetic portions and W is the magnetic portions were analyzed by the XRF and XRD methods.

For the further purification of nonmagnetic portion of the first processed portion was subjected to the second separation process. The chemical analysis of the second nonmagnetic portion was determined by XRF method. The result was given in Table 2 the second and the third lines. These results show that, magnesite content reached up to 91.03 % after the two times application of the wet magnetic separation process to the magnesite tailing sample. The process was very effective at 1.8 T for concentrating of high quality magnesite.

**Table 3** The effect of magnetic field on the sieve analysis.

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| Mag. intensity | Sample | -3.0 +2.0mm | -2.0 +1.0mm | -1.0 +0.50mm | -1.0 +0.25mm | -0.5 +0.10mm | -0.10mm |
| -- | As received | 12.21 | 40.21 | 26.73 | 13.82 | 4.95 | 2.08 |
| 0.1 T | NMP ( product) | 7.09 | 54.34 | 33.67 | 4.85 | 0.04 | 0.01 |
| 1.8 T | II.sep, II.NMP | 5.94 | 51.13 | 38.34 | 4.56 | 0.01 | 0.01 |
| II. sep. MP | 9.98 | 58.09 | 27.25 | 4.58 | 0.09 | 0.01 |

In Table 3, the second and the third lines show the beneficiation results of the starting sample after the high intensity wet magnetic separation process. Any processing of minerals is determined from physical and chemical properties. The chemical composition results of the magnetic and the nonmagnetic portion of the process were compared with the as-received sample. From the chemical composition point of view, there are big differences in iron content of all samples. The recovery of magnesite or the removal of iron bearing minerals from the magnesite tailing was successfully done and resulted considerable differences in the chemical compositions. Iron content in the nonmagnetic fraction that is called product is very low, deceased from 3.14 % to 0.38 %, but it was increased from 3.14 % to 6.98 % in the magnetic fraction. Unfortunately, iron content of magnesite is not zero value because of it is in the spinel form of lizardite structures 1M (Mg3(Si2O5)(OH)4), 1T ( trigonal pyramids, Mg2.82Fe0.07Al0.09)(Si1.94Al0.06)O5(OH)4), and 2H (hexagonal plates, Mg2.83Fe0.05Al0.10)(Si1.93 Al0.07 )O5(OH)4)) as seen consist of Al, Mg, Fe and Si. Lizardite is kaolinite-serpentine group mineral and displays poly types. The differences between lizardite phases come from octahedral and tetrahedral sheets structure. Al, Mg, Fe and Si control chemical composition when Fe where shows two valance states, involves the structure of lizardite sheets changes and becomes more complex. At higher magnetic intensity lizardite is separated from magnesite ore depending on iron in lizardite.

In order to evaluate the wet magnetic processing, the chemical composition, the thermal behavior and the X-ray diffraction patterns of the magnetic and the non-magnetic fractions of the processed samples were analyzed and compared with the as-received sample. From the chemical composition point, there are big differences in iron content of the processed samples. It is very low in the nonmagnetic portion after the first pass and is the lowest level in the second passé of the non-magnetic fraction. When compared with the thermal behavior of the samples, the degree of the weight loss are changing depending of the loss ignition content of them which are related with the carbonization of the phases in the samples.



**Figure 4** X-ray diffraction of the product (nonmagnetic portion at 1.8T).

The X-ray diffraction pattern of the nonmagnetic portion of the high intensity wet magnetic separation after the one pass at 1.8 T. As is shown in the identified peaks of the figure, all peaks belong to Mg related oxides and minerals such as MgCO3, MgO, (Ca, Mg)CO3. On the other hand, as a waste of the process, the magnetic portion of the separator was analyzed by the X-ray diffraction method that is presented in Figure 4. As is noted, the non and magnetic samples displays so different patterns and peaks on them. As seen in Figure 5, the magnetic portion contains different lizardite mineral forms that was iron bearing minerals in the magnesite tailing sample. The chemical analysis of the samples support the X-ray diffraction results on the base of iron oxide content. As it expected, the iron oxide content of the magnetic portion was the highest level in the three of the results. There was also color differences between the processed samples that the magnetic portion was in dark but the nonmagnetic portion was white-creamy.



**Figure 5** X-ray diffraction of the waste (the magnetic portion after the HIWMS process).

An inverse relationship exists between MgO and iron bearing minerals. When the MgO content is high, the iron content is decreased. The variation between the magnetic portions of the processed samples proves that the magnesite ore is referred to as a carbonate containing ore. The presence of iron oxide in the raw and the magnetic portions is associated with traces of iron containing minerals of lizardite.

The chemical compositions of both the magnetized and the non-magnetized portions of the samples were given in Table 1. As seen from these columns, the chemicalcompositions of the processed samples are quite different from the original sample. Iron content of magnesite sample can be removed by a number of chemical, physical and physicochemical methods. But magnetic separation is environment friendly method to remove any ferrous oxides from magnesite tailing because it is physical method without using any chemical agents. The magnetic portions have a high iron oxide content. MgCO3 content of the processed sample was increased up to 91.03 % after the wet magnetic operation but it was 62.46 % the waste of the process.

**3.3. Calcination and calcination behavior**

When compared with the thermal behavior of the samples, the degree of the ignition loss are important criteria for minerals that depending on organic content of them. The loss ignition of was calculated on the received, magnetic and the nonmagnetic portion of the processed samples, given in Table 4. As is expected, the magnetic portion was shown the lowest value in the samples that indicates the carbonate content of it is low. On the other side, the product sample has high loss ignition value which is related with the removal of carbonate content of the magnesite.

**Table 4** The loss of ignition content of the samples.

|  |  |  |  |
| --- | --- | --- | --- |
| Wt. % | T(Magnesite waste) | W (Magnetic ) | P (Magnesite) |
| Moisture | 4.67 | 5.05 | 3.31 |
| Loss of ignition | 37.01 | 17.02 | 48.00 |

The thermal behavior of the magnesite ore sample was investigated using thermal analysis method. TG/DTA curves of the sample was presented in Figure 6. Thermogravimetric mass loss changes of the received sample was determined by DTA and TGA. The sample displays four various weight loss zones depending whether the sample contains carbonate minerals. It was noticed that the first zone was 25-436 ˚C that of 1.75 % weight lost observed, but the huge amount of weight lost was occurred in the second zone at temperature between 436-650 ˚C that was 44.51 % of the total. The third one was between at temperature 650-826 ˚C was 2.4 % of weight loss was observed. The final zone was 826-1200 ˚C with a slow continuing loss was 0.22 %.

As seen from the TG curve, the received sample starts to decompose at 436 ˚C and continue until 826 ˚C. The mass loss between these temperatures was 47 %. After this temperature and up to 1200 ˚C total mass loss was 0.22 %. The total weight loss of the magnesite sample was found to be 48.91 % of total at temperature between 25-1200 ˚C.



**Figure 6** TG/DTA of the received magnesite ore sample.

In the DTA curve of the received magnesite sample, there were three endothermic. It noticed that the first peak of the DTA curve belongs to a small endothermic peak at approximately at 454 ˚C temperature probably due to dehydration of (OH) from the sample. The second one was sharp and main peak at 634.2˚C and the final endothermic was observed at temperature around 745.7 ˚C.

It should be noted that there was one exothermic peak at 650 and 826 ˚C. With carbonate, as a major structure, with little gangue minerals, the reactions will be in dissociation of carbonate of magnesite and dolomite. The peak at 629˚C is attributed to the decomposition of magnesite;

MgCO3=MgO + CO2 (1)

Pure MgCO3 dissociates at this temperature to form 47.8 % MgO and 52.2 % CO2. When heated sufficiently magnesia creates a crystal structure identical with natural periclase. As explained pervious parts, various calcinated magnesia are produced in different density and structure. The second peak at 634˚C is belong to the decomposition of dolomite;

(Ca, Mg) (CO3)2 = MgO + CaO +2CO2 (2)

Solid Ca/MgCO3 undergo thermal decomposition to give a solid magnesia or calcia powder and CO2 according to reactions 1 and 2. CaCO3 has to be calcinated at higher temperature than MgCO3.

The endothermic peak at 950 ˚C, can be explained by the dehydration of lizardite (3MgO·4SiO2·H2O) or clinocrisotile (Mg3Si2O5·(OH)4 the magnesite with the following reaction;

3MgO·4SiO2·H2O =3MgSiO3 + SiO2 + H2O (3)



**Figure 7** X-ray diffraction of the product (the nonmagnetic fraction) sample after calcination at 1000 ˚C for 2h.

After the high intensity magnetic separation of the received magnesite sample at 1.8 T, the non-magnetic fraction of the obtained sample is called product that was heat treated at 1000 ˚C in a muffle furnace in air atmosphere for 4h. in an alumina crucible. XRD pattern of the calcinated magnesia was given in Figure 7. The identified phase was only magnesia (MgO) and small amount of trace phases such as quarts (SiO2) and lime (CaO). As seen from Figure 7, any other impurity phases were not found.

**Table 5** Chemical analysis of the calcinated magnesia.

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
| MgO, % | SiO2, % | CaO, % | Fe2O3, % | Al2O3, % | Cr2O3, % | MnO, % |
| 85.39 | 7.72 | 6.14 | 0.63 | 0.09 | 0.63 | 0.02 |

The chemical analysis of the calcinated sample magnesia was presented in Table 5. Magnesia content has been increased significantly from 65.84 % to 85.39 % with decrease in amount of iron oxide from 5.58 % to 0.63 %. Silica ratio to CaO is around 1.12 % in the calcinated magnesia. This product is suitable for chemical and metallurgical applications [3, 4, 18].

**4. Conclusions**

This paper reviews basic characteristic and beneficiation methods of Kumaş magnesite ore waste by the wet-high intensity magnetic separation and calcination were investigated in laboratory conditions. It is shown that magnesite tailing consists of 77.69 % magnesite MgCO3 with a 3.14 % of Fe2O3. After the process, MgCO3 content was increased 91.03 % and iron content Fe2O3 content was decreased to 0.38 % as well as silica, alumina. The results of the characterization studies showed that the iron bearing mineral, lizardite, was the main impurity in the sample. The magnetic separation depends on a number of variables, such as, magnetic field, particle size, water content and iron bearing minerals or ferrous oxides. It was successfully separated at the magnetic field of 1.8 T from the magnesite portion. There are differences in chemical compositions, phases even on the colors of the processed samples. The obtained magnesite was subjected to calcination process at 1000 ˚C that that showed pure XRD pattern and 85.39 % MgO content was in it.

The composition of magnesite ore is stable and the removing of the impurities in it becomes more importantly. From this point of view, the physical separation methods of magnesite ore processing will have critical stage and importance for removing of iron bearing minerals. The high intensity wet magnetic separation (HIWMS) technique could be solution for the problem. It can be sued alone or combination with other techniques, because the demand for high grade magnesia will increased, depending on required raw magnesia material and applications.

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