#### Supplementary material to

# Application of response surface methodology to optimize the treatment process of high conversion of free fatty acids using (1R)-(-)-camphor-10--sulfonic acid and iron(III) sulphate

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Table S.: Box-Behnken design	for optimizing (	(1R)-(-)-camphor-10-sul	fonic acid catalyzed (	esterification
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Dup	Factor 1	Factor 2	Factor 3	Factor 4	Response
KUII	A: Catalyst dosage, wt.%	B: Methanol-to-oil molar ratio	C: Reaction temperature, °C	D: Reaction time, min	F / wt.%
1	1.25	14	60	50	0.75
2	1.25	14	60	50	0.72
3	1.25	14	40	30	1.73
4	1.25	14	40	30	1.7
5	2.25	8	60	10	1.57
6	2.25	8	60	10	1.5
7	1.25	8	40	10	2.76
8	1.25	8	40	10	2.8
9	1.25	8	40	50	1.78
10	1.25	8	40	50	1.77
11	2.25	2	60	30	4.1
12	2.25	2	60	30	4.3
13	2.25	14	60	30	0.44
14	2.25	14	60	30	0.4
15	0.25	2	60	30	5.1
16	0.25	2	60	30	4.9
17	2.25	8	40	30	1.88
18	2.25	8	40	30	1.81
19	1.25	8	80	50	1.8
20	1.25	8	80	50	1.79
21	1.25	14	80	30	0.96
22	1.25	14	80	30	1
23	0.25	8	80	30	3.72
24	0.25	8	80	30	3.7
25	1.25	8	60	30	1.39
26	1.25	8	60	30	1.41
27	1.25	2	60	50	3.31
28	1.25	2	60	50	3.29
29	0.25	8	60	50	3.86
30	0.25	8	60	50	3.85



Pup	Factor 1	Factor 2	Factor 3	Factor 4	Response
Kull	A: Catalyst dosage, wt.%	B: Methanol-to-oil molar ratio	C: Reaction temperature, °C	D: Reaction time, min	F / wt.%
31	2.25	8	80	30	1.6
32	2.25	8	80	30	1.56
33	1.25	8	60	30	1.39
34	1.25	8	60	30	1.41
35	0.25	8	40	30	4.87
36	0.25	8	40	30	4.8
37	2.25	8	60	50	0.44
38	2.25	8	60	50	0.42
39	1.25	8	80	10	2.98
40	1.25	8	80	10	3
41	1.25	8	60	30	1.39
42	1.25	8	60	30	1.41
43	0.25	8	60	10	5.99
44	0.25	8	60	10	6.2
45	1.25	8	60	30	1.39
46	1.25	8	60	30	1.41
47	1.25	14	60	10	2.12
48	1.25	14	60	10	2
49	1.25	8	60	30	1.39
50	1.25	8	60	30	1.41
51	0.25	14	60	30	3.74
52	0.25	14	60	30	3.69
53	1.25	2	60	10	5.05
54	1.25	2	60	10	5.15
55	1.25	2	40	30	4.14
56	1.25	2	40	30	4
57	1.25	2	80	30	2.68
58	1.25	2	80	30	2.8

### Table S.: Box-Behnken design for optimising iron (III) sulphate catalysed esterification

Dum	Factor 1	Factor 2	Factor 3	Factor 4	Response
Run	A: Catalyst dosage, wt.%	B: Methanol-to-oil molar ratio	C: Reaction temperature, °C	D: Reaction time, min	F / wt.%
1	1.25	14	60	50	0.75
2	1.25	14	40	30	1.73
3	2.25	8	60	10	1.57
4	1.25	8	40	10	2.76
5	1.25	8	40	50	1.78
6	2.25	2	60	30	4.1
7	2.25	14	60	30	0.44
8	0.25	2	60	30	5.1
9	2.25	8	40	30	1.88
10	1.25	8	80	50	1.8
11	1.25	14	80	30	0.96
12	0.25	8	80	30	3.72
13	1.25	8	60	30	1.39
14	1.25	2	60	50	3.31
15	0.25	8	60	50	3.86
16	2.25	8	80	30	1.6
17	1.25	8	60	30	1.39
18	0.25	8	40	30	4.87
19	2.25	8	60	50	0.44
20	1.25	8	80	10	2.98
21	1.25	8	60	30	1.39
22	0.25	8	60	10	5.99
23	1.25	8	60	30	1.39
24	1.25	14	60	10	2.12



Dun	Factor 1	Factor 2	Factor 3	Factor 4	Response
Run	A: Catalyst dosage, wt.%	B: Methanol-to-oil molar ratio	C: Reaction temperature, °C	D: Reaction time, min	F / wt.%
25	1.25	8	60	30	1.39
26	0.25	14	60	30	3.74
27	1.25	2	60	10	5.05
28	1.25	2	40	30	4.14
29	1.25	2	80	30	2.68
30	1.25	14	60	50	0.73
31	1.25	14	40	30	1.7
32	2.25	8	60	10	1.5
33	1.25	8	40	10	2.8
34	1.25	8	40	50	1.75
35	2.25	2	60	30	4
36	2.25	14	60	30	0.42
37	0.25	2	60	30	5
38	2.25	8	40	30	1.89
39	1.25	8	80	50	1.82
40	1.25	14	80	30	1
41	0.25	8	80	30	3.75
42	1.25	8	60	30	1.4
43	1.25	2	60	50	3.2
44	0.25	8	60	50	3.9
45	2.25	8	80	30	1.58
46	1.25	8	60	30	1.4
47	0.25	8	40	30	4.8
48	2.25	8	60	50	0.42
49	1.25	8	80	10	3
50	1.25	8	60	30	1.4
51	0.25	8	60	10	6
52	1.25	8	60	30	1.4
53	1.25	14	60	10	2.2
54	1.25	8	60	30	1.4
55	0.25	14	60	30	3.75
56	1.25	2	60	10	5
57	1.25	2	40	30	4.2
58	1.25	2	80	30	2.7

# Table S3. Optimization constraints for (1R)-(-)-camphor-10-sulfonic acid-catalyzed esterification

Name	Goal	Lower limit	Upper limit	Importance
A: catalyst dosage, wt.%	Minimise	0.25	1.5	2
B: molar ratio	Is in range	2	14	2
<i>C</i> : Temperature, °C	Minimise	50	60	2
D: Time, min	Is in range	10	50	2
F/ wt.%	Minimize	0.44	1	5

# Table S4. Solutions of optimization for (1R)-(-)-camphor-10-sulfonic acid-catalyzed esterification

Number	Catalyst dosage. Wt.%	Molar ratio	Temperature, °C	Time, min	F / wt.%	Desirability	
1	1.50	12.67	59.58	33.11	0.43	1.000	Selected
2	1.48	13.65	56.47	35.85	0.44	1.000	
3	1.50	12.76	53.68	42.04	0.43	1.000	
4	1.48	12.88	59.23	46.75	0.43	1.000	
5	1.49	13.54	59.63	33.44	0.43	1.000	

#### Table S5: Optimisation constraints for iron(III) sulphate used for esterification of ACPO

Name	Goal	Lower Limit	Upper Limit	Importance
A: Catalyst dosage, wt.%	Minimise	2	6	1
B: Molar ratio	Is in range	8	12	2
C: Temperature, °C	Minimise	60	80	1
D: Time, min	Minimise	100	200	1
F / wt.%	Minimize	0.75	3.7	5



Number	Catalyst dosage wt.%	Molar ratio	Temperature, °C	Time, min	<i>F /</i> wt.%	Desirability	
1	3.14	12.00	60.00	178.59	1.037	0.771	Selected
2	3.12	12.00	60.00	178.81	1.036	0.771	
3	3.17	12.00	60.00	178.60	1.031	0.771	
4	3.11	12.00	60.00	178.36	1.047	0.771	
5	3.14	12.00	60.00	179.18	1.024	0.770	

Table S6. Solutions of optimisation for iron (III) sulphate-catalysed esterification

Table S7. Specifications of biodiesel produced from ACPO compared with the standard limits

Ducacutica	Diadianal frame ACDO	EN 14214		ASTM D6751	
Properties	Biodiesel from ACPO	Test method	Limit	Test method	Limits
Ester content, mol.%	96.3	EN 14103	min 96.5	-	-
Monoacylglycerol content, mol.%	0.05	EN 14105	max 0.80	-	-
Diacylglycerols content, mol.%	0.025	EN 14105	max 0.20	-	-
Triacylglycerols content, mol.%	<0.01	EN 14105	max 0.20	-	-
Free glycerol content, mol.%	<0.01	EN 14105	max 0.02	ASTM D 6584	max 0.020 wt.%
Total glycerol content, mol.%	0.050	EN 14105	max 0.25	ASTM D 6584	max 0.240 wt.%
Water content, mg kg <sup>-1</sup>	473	EN ISO 12937	max 500	ASTM D 2709	max 0.050 vol.%
K content, mg kg <sup>-1</sup> -	max 1	EN 14108	max 5.0	UOP 391	max 5.0
P content, mg kg <sup>−1</sup>	max 7.10	EN 14107	max 10.0	ASTM D 4951	max 0.001 wt.%
Density (at 15 °C), kg m <sup>-3</sup>	867	EN ISO 3675	860 - 900	-	-
Flash point, °C	182	EN ISO 3679	120 °C min	ASTM D 93	130 - min
Cloud point, °C	16	-	-	ASTM D 2500	Not specified
Content of sulphated ash, wt.%	<0.005	ISO 3987	Max 0.02 mol.%	ASTM D 874	Max 0.020
Total contamination, mg kg <sup>-1</sup>	0.008	EN 12662	24 - max	-	-
Copper strip corrosion (3 h at 50 °C)	Class 1	EN ISO 2160	Class 1 rating	ASTM D130	No. 3 max

Table S8. Effect of recycling catalysts on the FFA reduction and conversion of FFA to FAME

Reused runs –	(1R)-(-)-camphor-10-sulfonic acid		Iron (III) sulphate		
	F / wt.% (final)	FFA conversion, %	FFA content reduction, wt.%	FFA conversion, %	
1	2.09	75.20	3.51	58.36	
2	3.67	56.46	4.88	42.11	
3	4.23	49.82	4.39	47.92	
4	5.46	35.23	4.70	44.24	
5	5.48	34.99	5.36	36.41	



*Figure S1.* The perturbation plot for optimizing 10-CSA-catalyzed esterification



Figure S2. Normal plot of residuals for optimizing 10-CSA- catalysed esterification



*Figure S3:* Contour plots for timising 10-CSA-catalysed esterification: (a) catalyst dosage and methanol-to-oil molar ratio, (b) catalyst dosage and reaction temperature, (c) catalyst dosage and reaction time





Figure S4. The perturbation plot for optimising iron(III) sulphate catalysed esterification



Figure S5. Normal Plot of Residuals for optimising iron III sulphate acid catalysed esterification





*Figure S6.* Contour plots for optimising iron III sulphate catalysed esterification: (a) catalyst dosage and methanol-to-oil molar ratio, (b) catalyst dosage and reaction temperature, (c) catalyst dosage and reaction temperature

